August 17-20, 2025, Anaheim, USA

IDETC/CIE 2025





Hybrid Powertrain Optimization for Regional Aircraft Integrating Hydrogen Fuel Cells and Aluminum Air Batteries

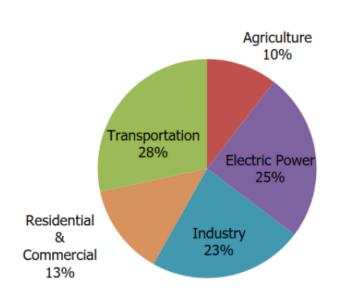


Harshal Kaushik¹, Ali Mahboub Rad¹, Korebami Adebajo², Sobhan Badakhshan¹, Nathaniel Cooper², Austin Downey², Jie Zhang¹

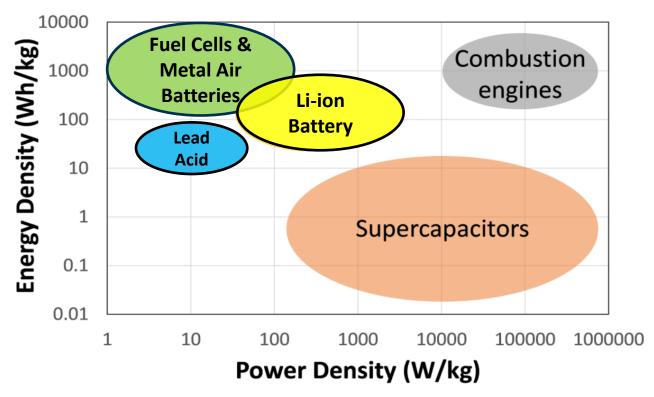
¹Dept. Of Mechanical Engineering., The University of Texas at Dallas ²Department of Mechanical, Aerospace, Civil Engineering, The University of South Carolina

Introduction and Motivation

- Reduce greenhouse emissions in transportation
- Lower ramp rate of the hydrogen fuel cell (slow to react to altering demands).
- Only batteries not sufficient for long range flights (low power/ weight ratio).

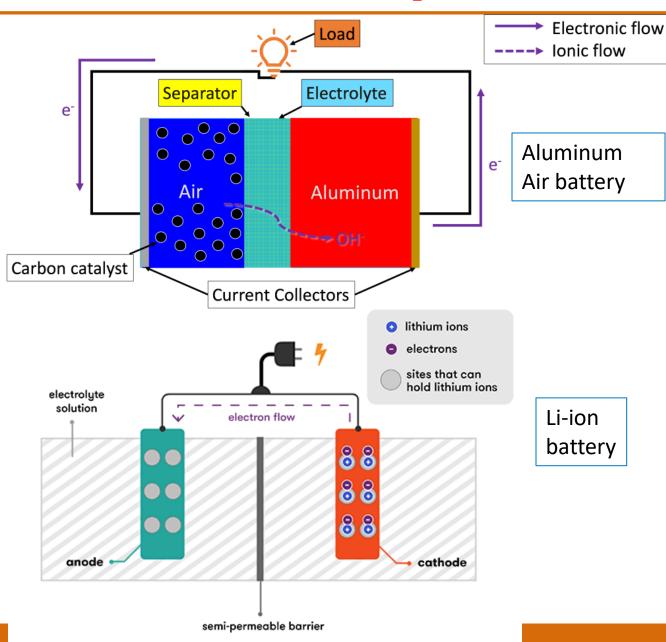


Total U.S. Greenhouse Gas Emissions by Economic Sector

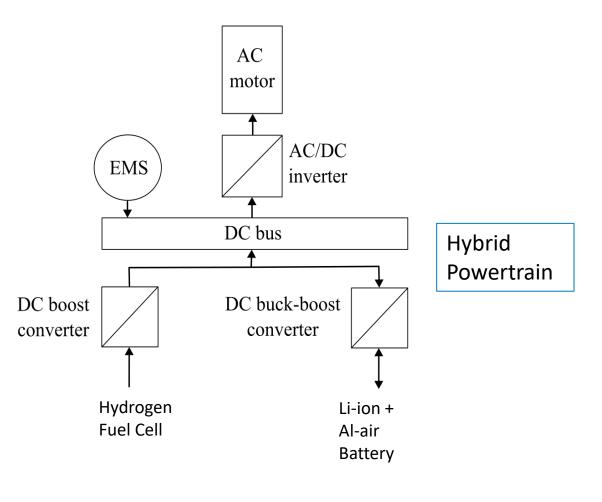


Source: U.S. Department of Energy, "Hydrogen Storage," Office of Energy Efficiency & Renewable Energy. [Online]. Available: https://www.energy.gov/eere/fuelcells/hydrogen-storage.

Introduction: Hybrid Powertrain



- Aluminum (Al) Anode and Air (Oxygen) Cathode.
- High Energy Density, Non-Rechargeable.



Outline

- ➤ Cessna 208 Specifications
- ➤ Mixed Integer Problem Formulation
- ➤ Experimental Set-up and Results
- ➤ Conclusion

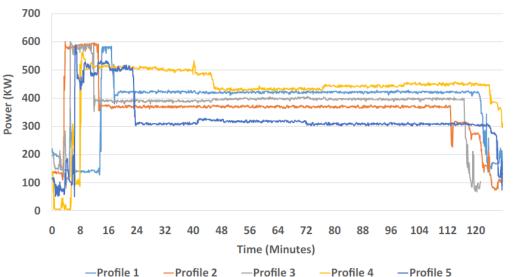


Cessna 208



Cessna 208





- Maximum Takeoff Weight: 8,000 lb (3,629 kg)
- Usable Fuel Weight: 2,224 lb (1,009 kg)
- Usable Fuel Volume: 332 gal (1,257 l)
- Basic Empty Weight: 4,730 lb (2,145 kg)
- Useful Load: 3,305 lb (1,499 kg)
- Maximum Payload: 3,070 lb (1,393 kg)
- Maximum Range: ~1,070 nautical miles (1,982 km)
- Maximum Flight Duration: 4-5 hours
- Engine (PT6A-114A) Weight: ~200 kg
- Seating Capacity: 9-14 passengers (plus 1-2 crew)

Power curves from the Cessna 208 for Columbia (South Carolina) to Richmond (North Carolina)

Objective Function and Decision Variables

- Multi-objective optimization: system sizing and power scheduling.
- Decision variables:
 - Hydrogen tank (L)
 - Fuel cell capacity (kWh)
 - Battery capacity (kWh)
 - Al-air capacity (kWh)

$$C_{H}^{\text{wt}} V_{H} + C_{FC}^{\text{wt}} E_{\text{fc}} + C_{\text{Li}}^{\text{wt}} E_{\text{Li}} + C_{\text{Al}}^{\text{wt}} E_{\text{Al}},$$

$$Weight of \\ \text{hydrogen} \\ \text{tank} \qquad Weight \\ \text{of Li-ion} \\ \text{battery} \qquad \text{battery}$$

$$\sum_{t \in T} P_{\text{fc}}^t + P_{\text{Li}}^t + P_{\text{Al}}^t.$$

TABLE 1: WEIGHT COEFFICIENT VALUES

Coefficient	C _H ^{wt} (kg/L)	C _{fc} ^{wt} (kg/kWh)	C _{Li} ^{wt} (kg/kWh)	$C_{\text{Al}}^{\text{wt}}$ (kg/kWh)
Value	1/11000	1.5	4	0.1234

Constraint Set

• To comply with payload limitations, the **total installed weight of all propulsion components is bounded** above by 1,200 kg.

$$C_{\rm H}^{\rm wt} V_{\rm H} + C_{\rm FC}^{\rm wt} E_{\rm fc} + C_{\rm Li}^{\rm wt} E_{\rm Li} + C_{\rm Al}^{\rm wt} E_{\rm Al} \le 1200,$$

TABLE 1: WEIGHT COEFFICIENT VALUES

Coefficient	C _H ^{wt} (kg/L)	C _{fc} ^{wt} (kg/kWh)	C _{Li} ^{wt} (kg/kWh)	C _{Al} (kg/kWh)
Value	1/11000	1.5	4	0.1234

• At every time step, the total power demand is exactly met by the combined output from the hydrogen fuel cell, Li-ion battery, and aluminum-air battery.

$$P_{\mathrm{fc}}^t + P_{\mathrm{Li}}^t + P_{\mathrm{Al}}^t = P_{\mathrm{dem}}^t, \quad \forall t \in T,$$

Constraint Set

 Available hydrogen supply is sufficient to meet the fuel cell energy demand throughout the entire flight.

$$V_{\rm H} \eta_{\rm fc} H_{\rm LHV} H_{\rm mass} \geq E_{\rm fc}$$
,

TABLE 2: HYDROGEN FUEL CELL PROPERTIES

Coefficient	$\eta_{ m fc}$	H _{LHV} (kWh/kg)	H _{mass} (kg/L)
Value	0.55	33.33	0.09

• Fuel cell ramp rate constraint: The power output from the hydrogen fuel cell over short periods (between any two timesteps) must remain within 10% of its rated capacity.

$$P_{\text{fc}}^{t_1} - P_{\text{fc}}^{t_2} \le 0.1 \ E_{\text{fc}}, \quad \forall t_1, t_2 \in T,$$

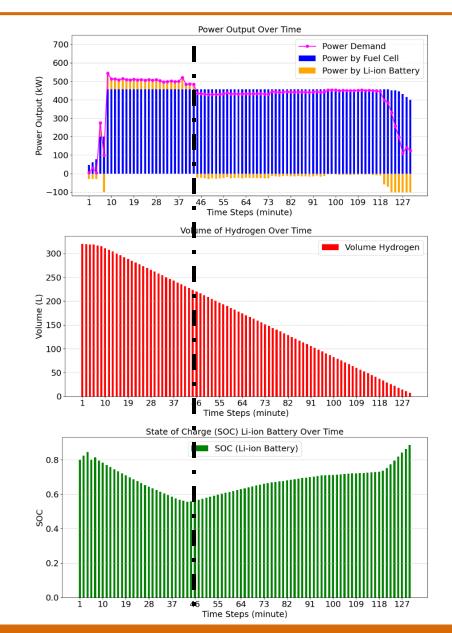
Constraint Set

- The battery's state of charge (SOC) changes dynamically based on how much energy is drawn over time.
- At any time t_1 , the **stored energy** is updated from time t_2 by **accounting for power consumed** over the interval.

$$SOC_{Li}^{t_1} E_{Li} = SOC_{Li}^{t_2} E_{Li} - P_{Li}^{t_1} \Delta t, \quad \forall t_1, t_2 \in T.$$

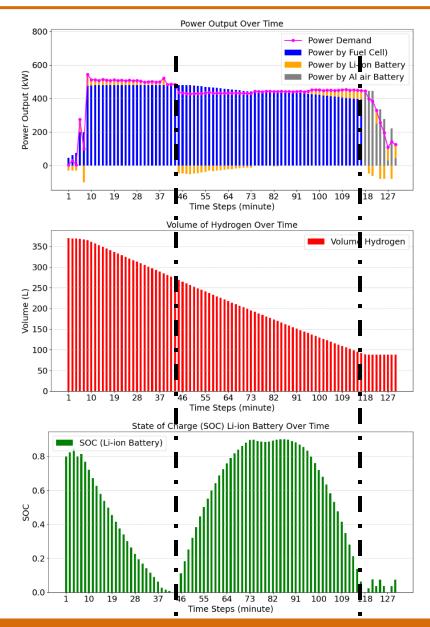
Experiment 1

- **Primary Power Source**: The hydrogen fuel cell serves as the main power provider throughout the flight, with lithiumion batteries acting as a complementary source.
- **Phase-Specific Optimization**: During the cruise, when power demands are relatively steady, the fuel cell fulfills most of the load.
- Battery-Assisted Smoothing: The Li-ion battery steps in to manage transient spikes and dips in power demand, ensuring smooth and stable energy delivery.
- Hydrogen Usage: The gradual depletion of hydrogen volume indicates consistent fuel consumption by the fuel cell.
- Battery State of Charge (SOC): The SOC curve confirms that the battery is effectively used to buffer variations and is recharged during low-demand phases.



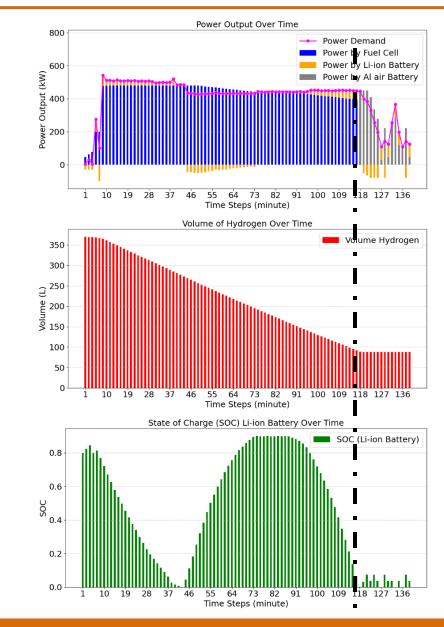
Experiment 2

- Scenario Setup: We consider a scenario where hydrogen volume drops below 20% of total capacity, posing safety risks. Aluminum-air battery is activated as a backup.
- Normal Operation Phase: Power is supplied by the hydrogen fuel cell and Li-ion battery. The fuel cell handles main power load during climb and cruise, while the battery smooths fluctuations.
- Critical Transition Phase: Once hydrogen falls below 20%, the fuel cell shuts down to preserve remaining fuel.
- Emergency Backup Activation: Aluminum-air battery takes over as the primary power source to ensure safe flight completion under depleted hydrogen conditions.



Experiment 3

- Scenario Setup: A rerouting scenario is considered in which the aircraft must perform a go-around and return to the runway due to events like a missed approach, poor visibility, or adverse weather.
- Normal Operation Phase: Initially, the system functions under planned conditions using the hydrogen fuel cell as the primary power source, with the lithium-ion battery assisting during power fluctuations.
- Critical Transition Phase: A deviation from the flight plan triggers an extended flight duration, requiring realtime energy management adjustments to handle the additional power and energy demands.



Optimal Sizing Results

TABLE 3: SIZING CONFIGURATIONS FOR HYBRID ENERGY SYSTEM COMPONENTS

Experiment	Fuel Cell	Li-ion Battery	Aluminum-air	Hydrogen	Powertrain
	capacity (kWh)	capacity (kWh)	battery capacity (kWh)	volume (L)	weight (kg)
Experiment 1	458	100	0	320	1200
Experiment 2	480	80	450	370	1142
Experiment 3	480	80	450	370	1142

Experiment 1:

- No aluminum-air battery used; only fuel cell and Li-ion battery components are sized.
- Powertrain reaches maximum allowable weight of 1200 kg, utilizing full design capacity.
- Hydrogen volume is limited to 320 L.

Experiment 2 and 3:

- Aluminum-air battery with 450 kWh capacity to support backup power needs.
- Fuel cell size increases slightly to 480 kWh, while Li-ion battery size decreases to 80 kWh.
- Hydrogen volume increases to 370 L, yet total system weight remains under the limit at 1142 kg.

Conclusion and Future Work

- **Hybrid Powertrain Development**: Designed a multi-source hybrid energy system for the Cessna 208 aircraft, integrating a hydrogen fuel cell, lithium-ion battery, and aluminum-air battery to enhance operational flexibility and safety.
- Optimization Framework: Formulated and solved a mixed-integer programming model that jointly optimizes component sizing and power scheduling across mission profiles.
- **Scenario-Based Validation**: Conducted rigorous simulations under nominal, hydrogen-limited, and emergency diversion scenarios using real-world flight data to validate system performance and robustness.

Path Forward:

- Stochastic Sizing: Future work will extend the sizing model to account for uncertainties in energy prices and environmental conditions.
- Robust Energy Planning: Focus on adaptive scheduling policies that generalize across diverse flight profiles and operational contingencies.

Thank You





